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Catalytic reduction of N_2O over steam-activated FeZSM-5 zeolite Comparison of CH₄, CO, and their mixtures as reductants with or without excess O_2

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Abstract

The catalytic reduction of N₂O by CH₄, CO, and their mixtures has been comparatively investigated over steam-activated FeZSM-5 zeolite. The influence of the molar feed ratio between N₂O and the reducing agents, the gas-hourly space velocity, and the presence of O₂ on the catalytic performance were studied in the temperature range of 475–850 K. The CH₄ is more efficient than CO for N₂O reduction, achieving the same degree of conversion at significantly lower temperatures. The apparent activation energy for N₂O reduction by CH₄ was very similar to that of direct N₂O decomposition (140 kJ mol⁻¹), being much lower for the N₂O reduction by CO (60 kJ mol⁻¹). This suggests that the reactions have a markedly different mechanism. Addition of CO using equimolar mixtures in the ternary N₂O + CH₄ + CO system did not affect the N₂O conversion with respect to the binary N₂O + CH₄ system, indicating that CO does not interfere in the low-temperature reduction of N₂O by CH₄. In the ternary system, CO contributed to N₂O reduction when methane was the limiting reactant. The conversion and selectivity of the reactions of N₂O with CH₄, CO, and their mixtures were not altered upon adding excess O₂ in the feed. © 2006 Elsevier B.V. All rights reserved.

Keywords: FeZSM-5; N₂O; Decomposition; Reduction; SCR; CH₄; CO; O₂; Tail-gases

1. Introduction

Nitrous oxide is a powerful greenhouse gas with 310 and 15 times the global warming potential of carbon dioxide and methane, respectively, and was included in the six-gas basket defined by the United Nations Framework Convention on Climate Change in Kyoto (1997) [1]. The harmful effect of N₂O in our environment is further aggravated by its indirect contribution to the ozone layer depletion as the main precursor of stratospheric NO_x [2,3]. Due to the anthropogenic action, the atmospheric concentration of N₂O experiences an annual growth rate of 0.3% (currently 310 ppb) [4], and strategies to control emission of this gas are being intensively explored and in some cases, developed and implemented.

 N_2O emissions that can be reduced in the short term are associated with chemical production and the energy industry

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[5,6]. In these sources, catalytic decomposition of N_2O into N_2 and O_2 is a cost-effective alternative to mitigate this harmful gas, and the identification of promising systems has involved substantial research efforts in the last decade [5,7-10]. A common denominator of N2O-containing tail-gases is the coexistence of other components (O₂, CO₂, NO_x, H₂O, SO₂, etc.), which often causes adverse effects on the catalyst due to inhibition or poisoning effects, thus limiting its practical application. Iron-containing zeolites are attractive catalysts for N₂O abatement, exhibiting a unique behavior when these components are present. This includes the insensitivity to O₂, the positive effect of NO and SO₂ on the rate of N₂O conversion, and a remarkable resistance towards deactivation by H₂O [6,11]. Besides, the addition of reducing agents decreases the operation temperature over iron-containing zeolites by selective catalytic reduction (SCR) [12-14]. The latter aspect is of consideration in order to achieve high conversions in low-temperature tail-gases.

Related to this, Delahay et al. [15] showed that CO was a more effective reductant for N_2O over Fe-beta zeolite (BEA

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structure) in the presence of excess oxygen than propene, ndecane, ammonia, and hydrogen. Within light hydrocarbons, Kögel et al. [16] concluded that propane presented higher activities than methane and propene for the simultaneous reduction of NO and N₂O over FeZSM-5 (MFI structure) in the presence of O₂. In support of this, van den Brink et al. [17] also showed that propane is a more effective N₂O reductant than methane over FeZSM-5 in mixtures simulating tail-gases from nitric acid plants, i.e., containing NO_x , O_2 , and H_2O besides N₂O. Contrarily, Kunimori et al. [18] have recently reported that CH_4 reduces N_2O at lower temperatures than C_2H_6 and C₃H₈ in the presence of O₂ over an ion-exchanged FeZSM-5 catalyst. In addition, this work also claimed that CH₄ is a more efficient reducing agent for N₂O than CO, although no explanation of this catalytic behavior was provided. The comparison between methane and carbon monoxide in Ref. [18] was made using mixtures with 950–1000 ppm N₂O and different concentration of reductants (1000 ppm of CO and 500 ppm of CH_4) and in the absence of O_2 . The stoichiometric amount of CH₄ required to reduce 1 mol of N₂O is, depending on the selectivity to CO and CO₂ (Eqs. (1) and (2)), 3-4 times lower than that of CO (Eq. (3)). In view of the different reducing power of CH₄ and CO and the excess of methane used in Ref. [18], a fair comparison between both reductants was not established:

$$3N_2O + CH_4 \rightarrow 3N_2 + CO + 2H_2O \tag{1}$$

$$4N_2O + CH_4 \rightarrow 4N_2 + CO + 2H_2O \tag{2}$$

$$N_2O + CO \rightarrow N_2 + CO_2 \tag{3}$$

In the present work, we have systematically investigated the performance of steam-activated FeZSM-5 in $N_2O + CH_4$ and $N_2O + CH_4 + CO$ mixtures, comparing it with the previously reported $N_2O + CO$ system over the same catalyst [19,20]. To this end, the reactions were investigated in a broad temperature range using different feed compositions and space velocities. The influence of adding O_2 in the feed mixtures was also studied.

2. Experimental

2.1. Catalyst preparation

Details on the hydrothermal synthesis of isomorphously substituted FeZSM-5 have been described elsewhere [21–23]. The as-synthesized sample was calcined in air at 823 K for 10 h and converted into the H-form by three consecutive exchanges with an NH₄NO₃ solution (0.1 M) for 12 h and subsequent air calcination. Finally the zeolite was activated in a flow of nitrogen and steam at 1 bar, using a partial steam pressure of 300 mbar and 30 ml STP N₂ min⁻¹ at 873 K for 5 h. Detailed characterization studies of the steam-activated FeZSM-5 (Si/Al = 31.3 and 0.67 wt.% Fe) identified various forms of extra framework species, including isolated iron ions and oligonuclear iron species in the zeolite pores, co-existing with iron oxide nanoparticles of 1–2 nm at the external surface of the zeolite crystal [22,23].

2.2. Activity tests

Activity measurements were carried out in a fixed-bed quartz reactor (4 mm i.d.) at atmospheric pressure, using 50 mg of catalyst (sieve fraction 125-200 µm, bed height 9 mm), and a gas-hourly space velocity (GHSV) of 10,000 or 90,000 h^{-1} . The effect of the feed composition was studied isothermally in gas mixtures with different partial pressures of N₂O (1.5 mbar), CH_4 (0.2 or 1.5 mbar), CO (0.2, 0.6, or 1.5 mbar), and O_2 (0 or 20 mbar) in He. Before reaction, the catalyst was pre-treated in He at 723 K for 2 h and cooled in that gas flow to the initial reaction temperature. The temperature was increased at intervals of 25 K in the range 475-850 K. This procedure was followed by a stepwise decrease of temperature in 25 K intervals. In this temperature range, deactivation of the catalyst was absent and up- and down-cycles lead to very similar activity curves. Generally, 1 h after a change of conditions (temperature and feed composition), the conversion levels were constant and considered as the steady state. Reactant and product gases were analyzed with a gas chromatograph (HP 6890) equipped with a thermal conductivity detector, using a Porapack Q column (for CH₄, N₂O, and CO₂ separation) and a Molsieve 13X column (for N₂, O₂, and CO separation).

Along the manuscript, feed mixtures are typically expressed using the ratio of partial pressures. For example, N₂O/ CH₄ = 1.5/1.5 denotes a binary reactant mixture containing 1.5 mbar of each gas with He as balance. Following this example, the molar ratio between reactants is indistinctively denoted as N₂O/CH₄ = 1.

3. Results and discussion

3.1. CH_4 versus CO as reductant for N_2O

Fig. 1 shows the N₂O conversion versus temperature over steam-activated FeZSM-5 in different feed mixtures. In the absence of reductant, i.e., direct N2O decomposition, the catalyst displays a significant N₂O conversion above 700 K and a complete conversion at 825 K. In the presence of equimolar amounts of methane or carbon monoxide, i.e., $N_2O/CH_4 = 1.5/$ 1.5 or $N_2O/CO = 1.5/1.5$ (Fig. 1a), the conversion of nitrous oxide shifts to lower temperatures (up to 150 K with methane). Both reducing agents start to display activity at the similar temperature (above 550 K). However, the slope of the conversion profile with CH₄ is much steeper than with CO. Accordingly, it can be stated that methane is more efficient in the low-temperature N₂O reduction than carbon monoxide. In this particular experiment, the required temperature for 100% N_2O conversion is ca. 75 K higher for CO (750 K) than for CH_4 (670 K). The superior low-temperature activity of methane for reduction of nitrous oxide is in agreement with recent work by Kunimori et al. [18].

Table 1 shows the apparent activation energies (E_a^{app}) for N₂O conversion in N₂O, N₂O + CH₄, and N₂O + CO mixtures. These were estimated around the inflection of the *X* versus *T* curves by assuming a plug-flow model and first-order reaction in N₂O. As it can be anticipated from the similar slope of the



Fig. 1. Conversion of N₂O vs. *T* over FeZSM-5 in different feed mixtures of N₂O + CH₄ and N₂O + CO (labels indicate partial pressures in mbar) at GHSV = 90,000 h⁻¹ and *P* = 1 bar. The conversion in direct N₂O decomposition (profile with open symbols) is also included.

conversion profiles, the apparent activation energies in direct decomposition and reduction by CH₄ are very similar (ca. 140 kJ mol⁻¹). The value of E_a^{app} in N₂O + CO decreases to 60 kJ mol⁻¹. Theses observations are in line with the literature. van den Brink et al. [17] observed that the direct N₂O decomposition and N₂O reduction by CH₄ and C₃H₈ over ion-exchanged FeZSM-5 have very similar apparent activation energies. Kapteijn et al. [24] and Pérez-Ramírez et al. [25] noticed a significant decrease of E_a^{app} in N₂O reduction by CO as compared to direct N₂O decomposition using FeZSM-5 and Fe-beta zeolites, respectively, with absolute values in good agreement with those reported here.

Table 1

Apparent activation energies for N_2O conversion in different feed mixtures, using 1.5 mbar of N_2O , CH_4 , and CO, 20 mbar O_2 , and He as the balance gas

Mixture	$E_{\rm a}^{\rm app}$ (kJ mol ⁻¹)
N ₂ O	140
$N_2O + CH_4$	135
$N_2O + CO$	60
$N_2O + CH_4 + CO$	110
$N_2O + CH_4 + O_2$	130
$N_2O + CH_4 + CO + O_2$	105

The different activation energy for N₂O conversion over steam-activated FeZSM-5 in $N_2O + CH_4$ and $N_2O + CO$ is likely related to the different nature of the active iron sites and reaction mechanism associated with the reducing agents. Recent studies using in situ UV/vis spectroscopy [20] and transient isotopic studies in a temporal analysis of products (TAP) reactor [26] have concluded that isolated Fe(III) species in extra framework positions of the zeolite are essential for N2O reduction by CO, according to their affinity to strongly coordinate carbon monoxide. On the other hand, several authors have concluded in the light of detailed mechanistic studies that oligonuclear iron-oxo clusters are preferred sites in the reduction of N₂O with light hydrocarbons such as CH₄ [18,27] and C₃H₈ [26,28]. Previously, some of us reported that CO is active over isolated iron sites [20], mainly present in the steam-activated Fe-silicalite catalyst used (ca. 70%). This sample proved to be more active for CO oxidation than for $C_{3}H_{8}$ oxidation with N₂O [26], which may suggest that oligonuclear iron species are more relevant for propane conversion. We could assume that methane and propane participate in N₂O reduction following a similar mechanism. This can be suggested from the excellent agreement between the work of Kunimori et al. [18] with $N_2O + CH_4$ and our recent work in the TAP reactor with $N_2O + C_3H_8$ [26]. Both studies have concluded the presence of two types of adsorbed atomic oxygen species in the reaction: nascent and thermally accommodated. Furthermore, as mentioned above, Kunimori et al. [18] attributed the activity of the $N_2O + CH_4$ reaction to binuclear species in FeZSM-5. In good agreement with the above reasoning, the steam-activated FeZSM-5 used in this work, which contains more oligonuclear iron species (ca. 60%) than isolated iron sites (ca. 30%) [20], is more active for N₂O reduction with CH₄ than with CO. According to this, the reduction of N₂O by CH₄ over FeZSM-5 seems to occur preferably over oligonuclear iron species, contrarily to the dominant role of isolated sites in the N₂O reduction by CO. Consequently, it is not appropriate to generalize that a certain reducing agent is more efficient than others, since its efficiency



Fig. 2. Conversion of CH₄ vs. *T* over FeZSM-5 in different feed mixtures (labels indicate partial pressures in mbar) at GHSV = $90,000 \text{ h}^{-1}$ and *P* = 1 bar.



Fig. 3. Selectivity to CO and CO₂ at GHSV = $90,000 \text{ h}^{-1}$ and P = 1 bar in different mixtures: (•) N₂O/CH₄ = 1.5/1.5, (•) N₂O/CH₄ = 1.5/0.2, and (•) N₂O/CH₄/O₂ = 1.5/1.5/20.

will be ultimately determined by the nature of the reductant and the distribution of the iron species in the zeolite.

When the reducing agent was the limiting reactant, i.e., N_2O/CH_4 or $N_2O/CO = 1.5/0.2$, the N_2O conversion profile experiences a plateau (Fig. 1b) at the temperature at which the reductant is consumed (ca. 725 K for CH₄, Fig. 2), and the conversion curve

gradually shifts to that of the direct N₂O decomposition. This plateau is also observed in the CH₄ conversion profile (at 30% conversion, Fig. 2), when N₂O is totally converted and the latter is the limiting reactant ($N_2O/CH_4 = 1.5/1.5$). This was also observed by Kunimori et al. [18] over ion-exchanged FeZSM-5 catalysts. These authors only investigated the $N_2O + CH_4$ reaction in excess of reducing agent, so that the conversion of N₂O reaches 100% before methane was totally converted. In order to establish a proper comparison of CH₄ and CO as N₂O reductants, the partial feed pressures were adjusted in order to have the same amount of reductant equivalents. This means, attending to the stoichiometry of Eqs. (1)–(3), having a 3–4 times lower CH₄ concentration in the feed mixture compared to CO. To this end, reactions were carried out using mixtures of N₂O/ $CH_4 = 1.5/0.2$ and $N_2O/CO = 1.5/0.6$ (see Fig. 1b). These mixtures exactly have the same reducing power assuming that the selectivity of the N₂O reduction by CH₄ yields CO with 100% selectivity. As seen in Fig. 3, this is only fulfilled at T < 550 K. Above this temperature, the CO selectivity gradually decreases in favour of CO2. However, it is clear that the efficiency of methane for N₂O reduction is superior to that of carbon monoxide. This can also be concluded by comparing the N₂O conversion at 625 K in N₂O/CH₄ = 1.5/0.2 (ca. 40%, solid circles in Fig. 1b) with that at the same temperature in $N_2O/CO = 1.5/1.5$ (ca. 25%, solid triangles in Fig. 1a).



Fig. 4. Partial pressure of N₂, O₂, CO, and CO₂ vs. *T* over FeZSM-5 in different feed mixtures (labels indicate partial pressures in mbar) at GHSV = 90,000 h⁻¹ and P = 1 bar.

Fig. 4 shows the partial pressures of reaction products (N_2, N_2) O₂, CO, and CO₂) associated with the experiments in different feed mixtures. As reported in our previous work [19], at molar N_2O/CO ratios ≤ 1 the amount of CO_2 formed equals the amount of N₂O decomposed and N₂ formed at all temperatures, with no formation of oxygen, in agreement with the stoichiometry of the reaction given in Eq. (3). At molar N_2O/CO ratios >1, O_2 is produced at temperatures where CO is consumed, and both direct N₂O decomposition and N₂O reduction by CO take place in the catalyst bed. In the case of N_2O reduction by methane, at $N_2O/CH_4 = 1.5/1.5$, no formation of O₂ was observed and the initial amount of carbon was balanced with that in the effluent, indicating that coke is not formed during the reaction. The selectivity to carbon monoxide (S(CO) = 75% at 675 K where N₂O conversion is complete (solid circles in Fig. 3)) is much higher than that of CO_2 . At $N_2O/CH_4 = 1.5/0.2$, the N_2 profile shows a plateau, when CH_4 is totally consumed (similarly to the $N_2O + CO$ system in Ref. [19]) and the selectivity to CO_2 reaches 100% above 700 K. The production of O₂ starts at 770 K, i.e., when the N₂O conversion profile shifts to that of direct N₂O decomposition.

Finally, the influence of the gas-hourly space velocity on the conversion during direct N_2O decomposition and N_2O reduction by CH₄ and CO over steam-activated FeZSM-5 was investigated using equimolar mixtures with 1.5 mbar of each reactive gas. The results in Fig. 5 show that the N_2O conversion profiles in all these reactions shifted ca. 50 K to lower temperature when the space velocity was reduced from 90,000 h⁻¹ (open symbols) to 10,000 h⁻¹ (solid symbols).

3.2. N_2O reduction by $CH_4 + CO$ mixtures

Fig. 6 shows the conversion of N_2O in the binary $(N_2O + CH_4 \text{ and } N_2O + CO)$ and ternary $(N_2O + CH_4 + CO)$ systems using different partial pressures of the reducing agents. In the case of mixtures where N_2O is the limiting reactant (excess of reductant), i.e., $N_2O/CH_4/CO = 1.5/1.5/1.5$, the addition of CO to the $N_2O + CH_4$ mixture does not affect the N_2O conversion profile. The CH₄ conversion slightly decreased from 30% to 20% in the presence of CO (Fig. 2). An increased CO₂ partial pressure was obtained when adding CO (Fig. 4c), indicating a higher CO₂ selectivity in the $N_2O + CH_4 + CO$ mixture as compared to the $N_2O + CH_4$ mixture.

When the reducing agent was the limiting reactant, as exemplified by the mixture of N₂O/CH₄/CO = 1.5/0.2/0.2, the N₂O conversion profile shows a plateau at temperatures at which CH₄ and CO are consumed, as described earlier for the binary systems (see products distribution in Fig. 4). The N₂O conversion in N₂O/CH₄/CO = 1.5/0.2/0.2 is significantly higher than in N₂O/CH₄ = 1.5/0.2 due to the contribution of CO in N₂O reduction. As shown in Fig. 2, the conversion of CH₄ does not change when adding CO (0.2 mbar) to the mixture N₂O/ CH₄ = 1.5/0.2 (see Fig. 2). The overall CO₂ concentration in Fig. 4c is the sum of the CO₂ coming from CH₄ and CO conversions. When both CH₄ and CO are consumed at 725 K, O₂ appears as a product of the direct N₂O decomposition (>750 K, Fig. 4d).



Fig. 5. Effect of the gas-hourly space velocity on the N₂O conversion vs. *T* over FeZSM-5 in equimolar feed mixtures (1.5 mbar of each reactive gas) of N₂O + CH₄ (circles), N₂O + CO (triangles), and N₂O (squares). GHSV = 90,000 h⁻¹ (open symbols) and 10,000 h⁻¹ (solid symbols).

3.3. Influence of O_2

The experiments of N_2O reduction presented so far were carried out in the absence of oxygen. Since relatively high concentrations of oxygen are often present in N_2O -containing tail-gases, it is important to investigate the catalytic performing upon adding excess O_2 in the feed. Fig. 7 shows the activity of



Fig. 6. Conversion of N₂O vs. *T* over FeZSM-5 in different feed mixtures (labels indicate partial pressures in mbar) at GHSV = $90,000 \text{ h}^{-1}$ and *P* = 1 bar.

FeZSM-5 in an equimolar $N_2O + CH_4 + CO$ mixture (1.5 mbar of each reactive gas) with or without the addition of excess O₂ (20 mbar) The conversions of N₂O and the reducing agents were not affected by the presence of O_2 in the temperature range investigated. In a similar way, the binary $N_2O + CO$ and $N_2O + CH_4$ systems were not affected by O_2 (not shown), confirming the selectivity of the reducing agents for N₂O on our particular catalytic system. As expected, the apparent activation energies for N₂O conversion do not change in the absence or presence of oxygen (see Table 1). The selectivity to CO and CO₂ upon methane conversion in the reaction of N₂O and CH₄ was not changed upon oxygen addition either (Fig. 3). Differently, the work of Kunimori et al. [18] concluded that the N₂O conversion over an ion-exchanged FeZSM-5 zeolite is shifted to higher temperature when 10 vol.% O₂ is present in the N₂O + CH₄ mixture. Curiously, this result was not elaborated or even mentioned by the authors. Besides, the selectivity to CO₂ increased with oxygen in the feed. At this stage, we do not have a clear explanation for this distinct behavior over these catalysts. However, it should be stressed that the different iron



Fig. 7. Effect of O_2 on the conversion of N_2O vs. *T* over FeZSM-5 in an equimolar feed mixture of $N_2O + CH_4 + CO$ at $GHSV = 90,000 \text{ h}^{-1}$ and P = 1 bar.

constitution in the materials, principally determined by the preparation approach applied, may directly explain the different catalytic performance. It is well known that the liquid ion-exchanged method of preparation (similar to that in Ref. [18,27]) differs to the steam-activation of isomorphously substituted FeZSM-5 applied here in nature and distribution of iron species as well as catalytic performance [11]. In addition, the oxygen concentration in Ref. [27] was 5 times higher than in this study.

4. Conclusions

Our comparative study of the selective catalytic reduction of N₂O by CH₄ or CO, and their corresponding mixtures over steam-activated FeZSM-5 has concluded that CH₄ is a more efficient reducing agent for N₂O reduction than CO. For example, complete N₂O conversion was achieved with methane at a temperature 80 K lower (670 K) than with carbon monoxide (750 K) at a molar N_2O/X ratio = 1 $(X = CH_4 \text{ or } CO)$. The apparent activation energy in the direct N₂O decomposition and N₂O reduction by CH₄ was very similar (140 kJ mol⁻¹), being significantly lower in N₂O reduction by CO (60 kJ mol⁻¹). The addition of CO to the $N_2O + CH_4$ system does not affect the N_2O conversion when methane is in excess with respect to nitrous oxide. At low partial CH₄ pressures, the N₂O reduction is shifted to higher temperatures, motivating the contribution of CO to the N₂O conversion. Our observations suggest that the reduction of N₂O by CH₄ and CO proceed via a markedly different reaction mechanism and might occur over different iron sites of the zeolite. The degree of conversion of the reactants and products selectivity in the binary and ternary systems investigated was not affected by the presence of oxygen in the feed.

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References

- Kyoto Protocol to the United Nations Framework Convention on Climate Change, Annex A, Kyoto, Japan, December 1997 (available on line at: http://unfccc.int/resource/docs/convkp/kpeng.pdf).
- [2] M.B. McElroy, J.C. McConnell, J. Atoms. Sci. 28 (1971) 1095.
- [3] P.J. Crutzen, J. Geophys. Res. 76 (1971) 7311.
- [4] J.T. Houghton, et al. (Eds.), Climate Change 2001, The Scientific Basis, Contribution of the Working Group I to the Third Assessment Report of the IPCC, Cambridge, 2001.
- [5] F. Kapteijn, J. Rodriguez-Mirasol, J.A. Moulijn, Appl. Catal. B 9 (1996) 25.
- [6] J. Pérez-Ramírez, F. Kapteijn, K. Schöffel, J.A. Moulijn, Appl. Catal. B 44 (2003) 117.
- [7] M.A. Wójtowicz, J.R. Pels, J.A. Moulijn, Fuel Process. Technol. 34 (1993)1.
- [8] S. Tanaka, K. Yuzaki, S. Ito, S. Kameoka, K. Kunimori, J. Catal. 200 (2001) 203.

- [9] J. Pérez-Ramírez, F. Kapteijn, G. Mul, J.A. Moulijn, J. Catal. 208 (2002) 211.
- [10] M.A. Wójtowicz, J.R. Pels, J.A. Moulijn, Fuel Process. Technol. 73 (1994) 1416.
- [11] J. Pérez-Ramírez, F. Kapteijn, G. Mul, X. Xu, J.A. Moulijn, Catal. Today 76 (2002) 55.
- [12] J. Pérez-Ramírez, F. Kapteijn, G. Mul, J.A. Moulijn, Appl. Catal. B 35 (2002) 227.
- [13] G. Centi, F. Vazzana, Catal. Today 53 (1999) 683.
- [14] S. Kameoka, T. Suzuki, K. Yuzaki, T. Takeda, S. Tanaka, S. Ito, T. Miyadera, K. Kunimori, Chem. Commun. (2000) 256.
- [15] G. Delahay, M. Mauvezin, A. Guzmán-Vargas, B. Coq, Catal. Commun. 3 (2002) 385.
- [16] M. Kögel, R. Mönnig, W. Schwieger, A. Tissler, T. Turek, J. Catal. 182 (1999) 470.
- [17] R.W. van den Brink, S. Booneveld, J.R. Pels, D.F. Bakker, M.J.F.M. Verhaak, Appl. Catal. B 32 (2001) 73.
- [18] T. Nobukawa, M. Yoshida, K. Okumura, K. Tomishige, K. Kunimori, J. Catal. 229 (2005) 374.

- [19] M.N. Debbagh Boutarbouch, J.M. García Cortés, M. Soussi El Begrani, C. Salinas Martínez de Lecea, J. Pérez-Ramírez, Appl. Catal. B 54 (2004) 115.
- [20] J. Pérez-Ramírez, M.S. Kumar, A. Brückner, J. Catal. 223 (2004) 13.
- [21] A. Ribera, I.W.C.E. Arends, S. De Vries, J. Pérez-Ramírez, R.A. Sheldon, J. Catal. 195 (2000) 287.
- [22] J. Pérez-Ramírez, F. Kapteijn, J.C. Groen, A. Doménech, G. Mul, J.A. Moulijn, J. Catal. 214 (2003) 33.
- [23] J. Pérez-Ramírez, G. Mul, F. Kapteijn, J.A. Moulijn, A.R. Overweg, A. Doménech, A. Ribera, I.W.C.E. Arends, J. Catal. 207 (2002) 113.
- [24] F. Kapteijn, G. Marbán, J. Rodríguez-Mirasol, J.A. Moulijn, J. Catal. 167 (1997) 256.
- [25] J. Pérez-Ramírez, J.C. Groen, A. Brückner, M.S. Kumar, U. Bentrup, M.N. Debbagh, L.A. Villaescusa, J. Catal. 232 (2005) 318.
- [26] J. Pérez-Ramírez, E.V. Kondratenko, M.N. Debbagh, J. Catal. 233 (2005) 442.
- [27] M. Yoshida, T. Nobukawa, S. Ito, K. Tomishige, K. Kunimori, J. Catal. 223 (2004) 454.
- [28] E.V. Kondratenko, J. Pérez-Ramírez, Appl. Catal. A 267 (2004) 181.